Drawing and estimation
Prepared, Arranged and Composed by:-Asad Iqbal

ASSignatent th 01
Question茾02:- Calculate Mälsial
Derrand is Bar Bordering Shedule. (ie Bricks, Sand, Cement, crush ie)


$D_{1}=3-6^{\prime \prime} \times 7-0$
Story He nigh $D^{\prime}=12^{\prime}$


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* Binder Bass are Placed with \#3@ $12 \mathrm{"c} / \mathrm{c}$
* length of Extra bars $=1 / 3$ of span.
, All walls are $9^{\prime \prime}$ Thick.
* Story Heighé $=12^{\prime}$

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1) Excavation :-
$\therefore 2 / 39^{\prime} 3^{\circ} \times 3^{\prime} 6^{\prime \prime} \times 4^{\prime} 0^{\circ}=1099$ cu. ft $3 / 14^{\prime} 3^{\prime \prime} \times 3^{\prime} 6^{\prime \prime} \times 4^{\prime} 0^{\prime \prime}=598.5 \mathrm{cu} . f t$ Total :- $1697.5 \mathrm{cu} . \mathrm{fe}^{2}$
) Lear :- $\{1: 4: 8\rangle$
$2 / 39^{\prime} 3^{\prime \prime} \times 3^{\prime} 6^{\prime \prime} \times 0-3^{\prime \prime}=68.6875 \mathrm{cu}$.ft
$3 / 14^{\prime} 3^{\prime \prime} \times 3^{\prime} 6^{\prime \prime} \times 0-3^{\prime \prime}=37.40 \mathrm{cu} \cdot$ ft Total :- 106.0875 cu. FT
2) $P C C:\{1: 2: 4)$
$2 / 39^{\prime \prime} \times 30^{\prime \prime} \times 0.6^{\prime \prime}=117.75 \mathrm{cu} \cdot \mathrm{Fi}$
$3 / 14^{\prime} 3^{\prime \prime} \times 30^{\prime \prime} \times 0-6^{\prime \prime}=64.125$ ar. Ft Molal $=181.875 \mathrm{cu} \cdot \mathrm{Ft}$
$\rightarrow$ SEep 1:-

$$
\begin{aligned}
2 / 39^{\prime \prime} 3^{\prime \prime} \times 2.27^{\prime} \times 0.6^{\prime \prime} & =88.3125 \text { cuff } \\
3 / 14^{\prime \prime} \times 2.27^{\prime} \times 0.6^{\prime \prime} & =48.09375 \text { cu. Fe } \\
\text { Toluca } & =136.40625 \text { cu. Fl }
\end{aligned}
$$

) Step 2:-
$2 / 39^{\prime} 3^{\prime \prime} \times 1.5^{\prime} \times 0-6^{\prime \prime}=58.875 \mathrm{w} . \mathrm{FC}$ $3 / 14^{\prime} 3^{\prime \prime} \times 1.5^{\prime} \times 0-6^{\prime \prime}=32.0625 \mathrm{cu} .5 \mathrm{CL}$

Total $=90.9375 \mathrm{cu} \cdot \mathrm{ft}_{\mathrm{t}}$

1) Brick work belem DAB:- $\{N S L\rangle$
$2 / 39^{\prime} 3^{\prime \prime} \times 9^{\prime \prime} \times 2.25^{\prime}=G H$

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* Back Fill:-

Excantion - all \{i.e leon +Pac $\overline{0}$ )

$$
\Rightarrow 1697-719.43 \Rightarrow \quad 977.75 \text { cu. } 5 t
$$

7) Brich work B.w NSL DDPC
$2 / 39^{\prime \prime} 3^{\prime \prime} \times 0.9^{\prime \prime} \times 0.6^{\prime \prime}=29.43 \mathrm{CF}$
$3 / 14.3^{\prime \prime} \times 0.99^{\prime \prime} \times 0-6^{\prime \prime}=16.03125$ CFA
Total $=45.46125 \mathrm{CA}$
8) Brick work Above DPC:-

2/39'3" $\times 0-9^{\prime \prime} \times 12^{\prime}=706.5$ CFf
\{stoy Heghi〉
$3 / 14^{\prime} 3^{\prime \prime} \times 0-9^{4} \times 12^{\prime \prime}=384.75 \mathrm{CF}$

* Door Deduction:-

$$
\begin{aligned}
& \text { 1. } 3^{\prime} 6^{\prime \prime} \times 7-0^{\prime \prime} \times 0-9^{\prime \prime}=18.375 \mathrm{CF} \\
& \text { 1/ } 41-0 \times 7^{\prime}-0^{\prime \prime} \times 0-94=21 \mathrm{CFt} \\
& \text { Total }=39.375 \mathrm{CF}
\end{aligned}
$$

* Net Brick Work:-

Brich wrus above DR-Door openings. 1091:25-39.375

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External Plaster:$2 / 40^{\circ}-0^{\circ \prime} \times 12^{\prime}-6^{\prime \prime}=10000644$ Story Height $=12^{\prime} \delta_{\text {mas }}$. Full then due to extimal.
$2 / 15^{\circ}-0^{\prime \prime} \times 12^{\prime}-6^{\prime \prime}=375$ SOFt

$$
\text { Total }=1375 \mathrm{sel} / 4
$$

- Door deduetims:-

Net External Plestos:-

$$
\Rightarrow 1375-52.5
$$

$$
=1322.5 \mathrm{~S} . \mathrm{A} \cdot \mathrm{~A}
$$

 Total $=1554 \mathrm{se} \cdot \mathrm{ft}$

$$
1 / 3-6^{\circ} \times 7^{\prime}-0^{6}=24.5 \mathrm{S8} \cdot \mathrm{Ft}
$$ $1 / 4^{\prime}-0^{\prime \prime} \times 7^{\prime}-0^{\circ}=28$ Si FF

NET Interne Plaster.

$$
\begin{aligned}
& \text { 1) } 3^{\prime}-6^{\circ} \times 7^{\prime}-0^{\circ}=24.5 \mathrm{sa} . \mathrm{Ht} \\
& \text { 1) } 4-0^{\circ} \times 7^{\circ}-0^{\circ}=28 \text { surf } \\
& \text { Total }=52.5 \text { sur. it }
\end{aligned}
$$

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Zevinery Plaston in (1.4)

"perer" =ict
Point.
Tolat $\Rightarrow 509.625$ S94t

Whider is almays eaual to the Pletre:i) Conorete:-

1) Coronite for 8bbi-(112:4)

1/ $4.3 \times 186$ Cly
 crmer)
ii) Conscle for lonici: $(1: 2: 4$ )
 1) $E_{x}$ iii) 9 m
$\qquad$ tuake oi9062s culft

* Constle for Dpein $\underset{7}{\text { class } B}\langle(12: 4)$

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i) Excavation :-
lent work $=1697 \mathrm{cft}$
Beck fill $=977.75 \mathrm{cff}$
Plats ii) BB Work:-
$45 \cdot 46+\binom{1091.25-39.375}{$ OR $1052 \cdot 62}+204.60$ OR 1052.62
$+136.40625+90.9375 \Rightarrow 1530.0245$
Step $1+$ Sep $2+B B$ below NSL $+B B$ B.W NSLAD every $\quad+B B$ wm above $D P C$ )
ii) Plaster :-
i) Extermal:- $\{1: 4\} \Rightarrow 1322.5 \quad 58.4$
ii) Imbemac: : $\{1: 6\rangle \Rightarrow 1506+$ ceiling Plaster $\{509.6 \times 1)$
v) Convele:- $\dot{N}^{2}=2015.625$ Sq. 7
$\dot{\gamma}$

* Lean $\{1: 4: 8\rangle=106.0875$ Cul.ffV
- Class $B:-\{1: 2: 4)=P C C+S l a 6+$ Lentil +D PL
$=181.875+387+5.90625+15.15627$
$=584.78125$ cu. 4

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T $6 / \mathrm{mut}$
MATERIALS I EMAND :men
Exertion.
Ecesis work $=1697$ Cf t
$1697 \Rightarrow 48.48$ culm


Consul: $\left\{\begin{array}{l}\text { (14.4:8 }\end{array}\right)$
wet volume $=106.08 \mathrm{CF}$
Dry volume of Conspire $\{1: 4: 8\rangle$
Cement:- $\qquad$

$$
1 / 13 \times 163.36=12.566 \text { cu. fA } \quad \text { AN } \frac{12.566}{1.25} \rightarrow 10.0528 \text { bags of camail. }
$$

- Sand:-

$$
4 / 13 \times 163.36=50.26551
$$

- Crush:-

$$
8 / 13 \times 163.36 \Rightarrow 100.529 \mathrm{Cft}
$$

- Consele :- Class B <1:2:4)
$w_{\text {of } 100,}=589.15625$ ct
Dy $\mathrm{vd}=\mathrm{s} 89.15625 \times 1.5 \mathrm{t} \rightarrow 908.5846$ cf
*Cement:-
$1 / 7 \times 908.5846=129.797844 \Rightarrow \frac{129.7978}{1.25}$

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Send: $\quad 2 / 7 \times 908.5846=259.59<\mathrm{ft}$
couch: $4 / 7 \times 908.5846=519.1912$ c 7
Brick wren :-
Total $=1530.02 \mathrm{ct} /$ Convesser faction. Bricks $=1530.02 \times 13.5$ $\times 13.5$

$$
=20653.8255
$$

Nature.
Morton :- $(1: 6$
wee nor. of Morton:-
$30 \%$ of $B B$ is Moth en.

$$
\begin{aligned}
& 1529.913 \times 30 \Rightarrow 458.9739 \\
& \text { mantes } \frac{\times 30}{100} 458.9729 \text { cs }
\end{aligned}
$$

So, wet monks 100458.9739 CA of Volume of Mortor $=$
$458.9739 \times 1.27$

$$
=582.89 \overline{\mathrm{CF}}
$$

mane:-

$$
1 / 7 \times 582.89=83.27
$$

nd: $-6 / 7 \times 582.89=499.62<91$

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= Coment

$$
1 / 5 \times 69.976=9.998 \text { cou- } 7
$$

Sarnal :-

$$
4 / 5 \times 69.976=55.97748,00
$$

NUP $=$ Plests $\{1: 6)$
o wet vot:- sous.barscff

$$
2015.625 \times-0417 \Rightarrow 83.498 \text { en. } 74
$$

$\qquad$

- Dry voti-
$83.998 \times 1.27 \Rightarrow 106-6=146 \cdot 0$.
- Cemenie.
$\square$

- Sande

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- $a^{\circ}$
i) Cement:-
$7 \quad \Rightarrow \quad 12.56+129.79+83.27+13.99+15.204$

$$
\begin{gathered}
\text { = } 254.814 \text { cu. If } \\
\text { No. of bags of cement }=\frac{254.814}{1.25} \Rightarrow 204 \text { bags } \\
204 \text { bags Ans. }
\end{gathered}
$$

b) Sand:-

$$
\begin{aligned}
& \Rightarrow 50.26+259.59+55.9846+\frac{91.43+499.62}{975 \mathrm{cft}} \\
& =959.63 \mathrm{cu} . \mathrm{ft}^{9}
\end{aligned}
$$

1) rush - (Agrregei)

$$
\begin{aligned}
& \Rightarrow 100.52+519.19
\end{aligned}
$$

$$
\begin{aligned}
& \text { or } 625 \text { cu.ft }
\end{aligned}
$$

Bricky:-

$$
20653.83 \text { brides. }
$$

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Estimaluot of Reinforcing Steed:-

1) Main Steel:-

Distribution Steel.


Now $1050^{\circ} \times 3020 \mathrm{~kg} / \mathrm{st}$

$\Rightarrow 317.14 \mathrm{~kg}$

*3 e9"clc
$2 / 21 / 20^{\circ}-0^{\circ}=840^{\prime}$ converting
Hew 840 ㅈ. 170 88/5t

243.64 kg .

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炈/ft \#4@6" $\mathrm{C} / \mathrm{c} \ddagger$
? MID of Room $\quad$, $\frac{40}{3}=13.3$

$$
\left(\begin{array}{l}
\text { No. Of Bass:- } \\
\frac{\text { chess }_{\text {Span }}}{\text { Spain }}+1 \\
14-6^{\prime \prime}
\end{array}\right.
$$

$\therefore 22400{ }^{\prime} \times \cdot 3020 \mathrm{~kg} / \mathrm{st}$ $\frac{6^{4}}{}+1=30$
120.8 kg
iv) Binder Bard:-\#
*3@ 12 " $/ \mathrm{C}$. Given in Start
$1 / 8 / 15$
$\square$
$\Rightarrow 240^{\prime} \times \cdot 170$ K8/Ft $\Rightarrow 40.8 \mathrm{~kg}$

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= Comertag
$225^{\prime} \times 170 \Rightarrow 36.25 \mathrm{~kg}$

$$
38.25 \mathrm{~kg}
$$

$$
\begin{aligned}
& \text { r Convisin Facture \#3 } \\
& .170 \mathrm{~kg} / 5 \mathrm{y} \\
& \begin{array}{l}
\# 4 \\
.3025 \mathrm{~kg} / \mathrm{s}
\end{array}
\end{aligned}
$$

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$\therefore$ \#3 E Total length $=1785^{\prime}$
\#4 2 Total long Ho $=2726.2^{\prime}$
Ad Total Wight $=1127.63 \mathrm{~kg}$
$d_{n}$

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BB work Fist seep:-

$$
\begin{aligned}
& 2 / 20^{\prime}-0^{\prime \prime} \times 1-101^{\prime \prime} \times 0^{\prime \prime}-6^{\prime}=52.5 \mathrm{qf} \\
& 2 / 4^{\prime}-3^{\prime \prime} \times 1^{\prime}-6^{\prime \prime} \times 0^{\prime}-6^{\prime \prime}=13.875 \mathrm{ff} \\
& 1 / 9^{\prime}-3^{\prime \prime} \times 1^{\prime}-10^{\prime \prime} / 2^{\prime \prime} \times 0^{\prime}-6^{\prime \prime}=8.6710 \mathrm{ft}
\end{aligned}
$$

$$
75.0468 \mathrm{cff}
$$

BB work and step:-

$$
\begin{aligned}
& 2 / 27^{\prime}-7 \frac{1}{2} \text { "1 } \times 1^{\prime}-6^{\prime \prime \prime} \times 0^{\prime}-6^{\prime}=41.4375 \mathrm{ft} \\
& 2 / 9^{\prime}-7 / 2^{\prime \prime} \times 1^{\prime}-1_{2}^{\prime \prime} \times 0^{\prime}-6^{\prime \prime}=10.8281 \mathrm{eft} \\
& 1 / 9^{\prime}-71 / 2^{\prime \prime} \times 1^{\prime}-6^{\prime \prime} \times 0^{\prime}-6^{\prime \prime}=7.2187 \mathrm{ft}
\end{aligned}
$$

$$
59.4843 \mathrm{ctt}
$$

BB WHK below NSL:-

$$
2 / 27^{\prime}-3^{n} \times 1^{\prime}-1 \frac{1}{2}^{\prime \prime} \times 2^{\prime}-3^{\prime \prime}=137.4331
$$

2) $10^{\prime}-0^{\prime \prime} \times 0^{\prime}-4^{\prime \prime} \times 2^{\prime}-3^{\prime \prime}=33.75$
3) $\left.10^{\prime}-0^{\prime \prime} \times 0^{\prime}-4 \frac{1}{2}{ }^{4} \times 1\right)^{2}-7^{2}=\frac{4.6875}{1763906 \mathrm{c}}$

$$
\begin{aligned}
& \text { Lean }(1: 4: 0) \\
& \text { 2/ } 29^{\prime}-7 \frac{1}{2}{ }^{\prime \prime} \times 3^{\prime}-6^{\prime \prime} \times 0^{\prime}-3^{\prime \prime}=51.843 \mathrm{eft} 4 \mathrm{wo} \\
& \text { 2) } 7^{\prime}-7 \frac{1}{2} 11 \times 3^{\prime}-0^{\prime \prime} \times 0^{\prime}-3^{\prime \prime}=11.4375 \text { ff Sw } \\
& \text { 1) } 7^{\prime}-7^{\prime \prime} 2^{\prime \prime} \times 3^{\prime}-0^{\prime \prime} \times 0^{\prime}-3^{\prime \prime}=5.7187 \text { qt } \\
& \text { P.C.C }(1: 2: 4) \\
& \text { 2/ } 29^{\prime}-1 \frac{1}{2} 11 \times 3^{3}-0^{\prime \prime} \times 0^{\prime}-6^{\prime \prime}=87.375 \mathrm{ft} 4 \mathrm{w} \\
& 2 / \theta^{\prime}-1 \frac{111}{2} \times 1^{\prime}-10 / 2^{\prime \prime} \times 0^{\prime}-6^{\prime \prime}=15.2343 \mathrm{ft} 8 \mathrm{sw} \\
& 1 / 8^{\prime}-c_{2}^{\prime \prime} \times 2^{1}-3^{\prime \prime} \times 0^{\prime}-6^{\prime \prime}=9 \cdot 1406 \text { fe sw }
\end{aligned}
$$

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Backfill:-

$$
\begin{aligned}
& =1081 \cdot 125-491.67 \\
& =589.4542 \mathrm{cft}
\end{aligned}
$$

BB work \&/w NSL \& ope:-

$$
\begin{aligned}
2 / 27^{\prime}-3^{\prime \prime} \times 1^{\prime}-1 \frac{1}{2} 1 \prime \times 0^{\prime}-6^{\prime \prime}= & 30.6562 \mathrm{qf} \\
2 / 10^{\prime}-0^{\prime \prime} \times 0^{\prime}-9^{\prime \prime} \times 0^{\prime}-6^{\prime \prime}= & 7.5 \mathrm{ff} \\
1 / 10^{\prime}-0^{\prime \prime} \times 0^{\prime}-4 \frac{1}{2} \times 0^{\prime}-6^{\prime \prime}= & 1.975 \mathrm{cft} \\
& 1 \\
& 40.0312
\end{aligned}
$$

BB work above APc:-

$$
\begin{aligned}
& \text { 2) } 27^{\prime}-3^{\prime \prime} \times 1^{1}-1 \frac{1}{2}^{\prime \prime} \times 10^{\prime}-0^{\prime \prime}=613.125 \mathrm{fft} \\
& \text { 2/ } 10^{1}-0^{\prime \prime} \times 0^{\prime}-9^{\prime \prime} \times 10^{\prime}-0^{\prime \prime}=150 \mathrm{cft} \\
& \text { 1/ } 10^{1}-0^{\prime \prime} \times 0^{1}-4 \frac{1}{2} 4 \times 10^{\prime}-0^{\prime \prime}=37.5 \mathrm{cft} \\
& \\
& 800.625 \mathrm{ct}
\end{aligned}
$$

Deduction:-

$$
\begin{aligned}
& 2 / 4^{\prime}-0^{\prime \prime} \times 7^{\prime}-0^{\prime \prime} \times 0^{\prime}-9^{\prime \prime}=42 \mathrm{fft} \\
& 1 / 3^{\prime}-6^{\prime \prime} \times 7^{\prime}-0^{\prime \prime} \times 0^{\prime}-4 \frac{1}{2}=9.1075 \mathrm{ff} \\
& 7 / 4^{\prime}-0^{\prime \prime} \times 3^{\prime}-0^{\prime \prime} \times 1^{\prime}-1^{\prime \prime}=13.5 \mathrm{ft} \\
& 1 / 2^{\prime}-0^{\prime \prime} \times 2^{\prime}-0^{\prime \prime} \times 1^{\prime}-\frac{1}{2} \frac{1 \prime}{}=4.5 \mathrm{ft}
\end{aligned}
$$

Net $B B$ Work

$$
800.625-65.1875
$$

$$
=731.4375 \mathrm{ft}
$$

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D.P.C:- $(1: 2: 4)$
2) $27^{\prime}-3^{\prime \prime} \times 1^{\prime}-1 \frac{1}{2}^{\prime \prime} \times 0^{\prime}-2^{\prime \prime}=10.2391^{\prime \prime} \mathrm{fft}$
a) $10^{\circ}-0^{\prime \prime} \times 0^{\circ}-9^{\prime \prime} \times 0^{\prime \prime} \times 0^{\prime}-2^{\prime \prime}=0.626 \mathrm{cft}$
lintal:- $(1: 2: 4)$

External pluster (1:4):-- $\frac{15.17 \mathrm{Cbt}}{15012 \text { oft }}$

$$
\begin{aligned}
2 / 26^{\prime}-10^{\frac{1}{11}} \times 10^{\prime}-6^{\prime \prime} & =564.375 \mathrm{sft} \\
2 / 12^{\prime}-3^{11} \times 10^{\prime}-6^{11}= & 257.25 \mathrm{sft} \\
& + \\
& 921.625 \mathrm{sft}
\end{aligned}
$$

oeduction:-

$$
\begin{aligned}
& \text { 2) } 4^{\prime}-0^{\prime \prime} \times 7^{\prime}-0^{\prime \prime}=56 \mathrm{sft} \\
& \text { 1/ } 4^{\prime}-0^{\prime \prime} \times 3^{\prime}-0^{\prime \prime}=12 \mathrm{sft} \\
& \text { 1/ } 2^{\prime}-0^{\prime \prime} \times 2=0^{\prime \prime}=4 \mathrm{sft}
\end{aligned}
$$

Net external plester. 72 sft

$$
=821 \cdot 625-72
$$

$$
=749.625 \mathrm{sff}
$$

$$
\begin{aligned}
& \text { 2/5 } 5^{\prime}-6^{\prime \prime} \times 0^{\circ}-9^{\prime \prime} \times 0^{\prime}-9^{\prime \prime}=6.1875 \mathrm{cft} \\
& \text { 1/ } 5^{\prime}-0^{\prime \prime} \times 6^{\prime}-4 \frac{111}{2} \times 0^{\circ}-9^{\prime \prime}=1.4062 \text { off } \\
& 1 / 5^{\prime}-6^{\prime \prime} \times 1^{\prime}-\frac{1}{2} 11 \times 0^{\prime}-9^{\prime \prime}=4.6406 \mathrm{ff} \\
& \text { 1/3-6 } 3^{\prime \prime} \times 1^{1}-1 \frac{1}{2} \times 0^{\prime \prime}-7^{\prime \prime}=2.9531 \mathrm{cft}
\end{aligned}
$$

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Internal plaster $(1: 6)$ :-

$$
\begin{aligned}
\text { 2) } 25^{\prime}-0^{\prime \prime} \times 10^{\prime}-0^{\prime \prime} & =500 \text { set } \\
\text { 4) } 10^{\prime}-0^{\prime \prime} \times 10^{\prime}-0^{\prime \prime}= & 400 \text { soft } \\
& \frac{400 \text { sift }}{}
\end{aligned}
$$

Deduction:-

$$
\begin{aligned}
2 / /^{\prime}-0^{\prime \prime} \times 7^{\prime}-0^{\prime \prime} & =56 \mathrm{sff} \\
4 / 3^{\prime}-6^{\prime \prime} \times 7^{\prime}-0^{\prime \prime} & =24.5 \mathrm{sft} \\
1 / 4^{\prime}-0^{\prime \prime} \times 3^{\prime}-0^{\prime \prime} & =12 \mathrm{sft} \\
1 / 2^{\prime}-0^{\prime \prime} \times 2^{\prime}-0^{\prime \prime} & =4 \mathrm{sft} \\
& \frac{1}{}
\end{aligned}
$$

Net internal plasta:-

$$
\begin{aligned}
& =900-96.5 \\
& =80.35 \mathrm{sft}
\end{aligned}
$$

Ceiling penscer:- (1:4)

$$
\text { 1/15-1 } 5^{\prime \prime} \times 10^{\circ}-o^{\prime \prime}=150 \mathrm{sft}
$$

$$
1 / 10^{\prime}-0^{\prime \prime} \times 10^{\prime}-0^{\prime \prime}=100 \mathrm{sft}
$$

concrete roof slate:- (1:2:4)

$$
26^{\prime}-10 \frac{1}{2} 11 \times 12^{\prime}-3^{\prime \prime} \times 0^{\prime}-6^{\prime \prime}=164.6093 \mathrm{ft}
$$

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Summery:-
(1) Earth work:-

$$
\begin{aligned}
& 108 \cdot 125 \text { yt } \\
& \text { Excavation }=159.4542 \text { fit }
\end{aligned}
$$

$$
\begin{aligned}
& \text { Excavation }=1081.128 \text { en } \\
& \text { Bock fill }=589.452 \text { yet }
\end{aligned}
$$

() concrete:-

Lean $(1: 4: 8)=68.9992$ ft $p \mathrm{pl}^{2}$
$\operatorname{cosin}(1: 2: 4)=13.7812+13.3703+164.6093+111.7499$
(3) BB work:-
$75.0468+59.4043+176.3906+40.0312+731.4325$ $=1002.3904 \mathrm{cft}$
(4) pester: - $4494^{2}$ cons perm 94962
cutting $(1: 4)=\frac{02.625+258}{203.5}=2071.625 \mathrm{eft}$
enteral $(x .6)=803.5$ st +8 int
Concrete $(1: 2: 4)$..
any wight $=303510 \times 154)=467.40 \mathrm{ckt}$
cement $=1 / 7 \times 467.401=66.76 \mathrm{cft}$
$\frac{66.76}{(25)}=53.41$ bags
Gand $=4 / 7 \times 46740=133.41 \mathrm{ft}$
utporegate $=4 / 7 \times 467.40=267.045$ ff t

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plester $(1: 4)$ :-


$$
\text { Sened }=4 / 5 \times 56.711=45.3600 \mathrm{cft}
$$

plester (1:6):-
axd volumase $803.5 \times 0.04167=33.4818 \mathrm{ft}$
or Volume $=33.4810 \times \xrightarrow{1.27}$
comant $=1 / 7 \times 42 \sqrt{2}=6.074 \mathrm{gt}$
$\frac{6.074}{1 x}=4.059$ bey 5
sond $=6 / 7 \times 4252=36.44 \mathrm{gt}$

$$
\begin{aligned}
& \text { verumon }=41.65 \times(1.27) \\
& \begin{aligned}
\text { canount }=\frac{1 / 5 \times 56.711}{} & =11.342 \mathrm{ff} \\
\frac{11.352}{1.25} & =9.073 \mathrm{ff} \text { tegs }
\end{aligned}
\end{aligned}
$$

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Concrete $(1: 4: 0)$ :-
cory wing $=68.9992 \times 1.54=106.25 \%$
cement $=1 / 13+106 \cdot 25=0.173 \mathrm{qt}$ $\frac{0.173}{125}=6.539$ begs
sand $=4 / 13 \times 106.25=32.69 \mathrm{gt}$
Agteyple $=8 / 13 \times 106.25=65.38 \mathrm{gf}$
BB work
No of bricks $=1082 \cdot 3904+135=1465$
mat to ( 1.0 ) $30^{\circ}$ of motion is is revile wet velum of mortar $0.3 \times 108238=324.717$

Dry velum $=324717 \times 1.27$ 412.59 ff cement $=\frac{1 / 7 \times 412.39}{\frac{50.92}{125}}=58.972$ oft Sand $=6 / 7 \times 412.39=353.477$

Drawing and estimation
Prepared, Arranged and Composed by:-Asad Iqbal

Material demand:-

$$
\begin{aligned}
& \text { Cement } \\
& \begin{aligned}
&=4.859+9.073+47.13+6.539+53.419 \\
&=121.02 \\
& \text { Sand } \\
&=\begin{array}{l}
36.44+45.3698+353.477+32.69+135.52 \\
=
\end{array} \\
& 603.495 \mathrm{ft} \\
& \text { Crush } \\
&= 271.049+65.38 \\
&= 336.429 \mathrm{cft} \\
& \frac{\text { Bricks }}{14613}
\end{aligned}
\end{aligned}
$$

+ No of bricks =
* Aggregate $=$ 14650
+ Sand = 350 eft
* Cement $=$ 122 bags

